

WORLD INTELLECTUAL PROPERTY ORGANIZATION  
International Bureau



(51) International Patent Classification <sup>6</sup> : C03C 25/02, G02B 6/44, C09D 11/10		A1	(11) International Publication Number: <b>WO 98/50317</b>
			(43) International Publication Date: 12 November 1998 (12.11.98)
(21) International Application Number: PCT/NL98/00254		(81) Designated States: AU, BR, CA, CN, ID, JP, KR, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).	
(22) International Filing Date: 6 May 1998 (06.05.98)			
(30) Priority Data: 60/045,746 6 May 1997 (06.05.97) US 1007933 30 December 1997 (30.12.97) NL		<b>Published</b> <i>With international search report.</i>	
(71) Applicant: DSM N.V. [NL/NL]; Het Overloon 1, NL-6411 TE Heerlen (NL).			
(72) Inventors: ZAHORA, Edward, Paul; 115601 Walterlane, Naperville, IL 60564 (US). MURPHY, Edward, Joseph; 742 South Mitchel, Arlington Heights, IL 60005 (US). SZUM, David, Michael; 646 North Oaklawn, Elmhurst, IL 60126 (US). VAN DEN BURG, Johannes, Cornelis; Christiaan Weenigstraat 76, NL-3151 CV Hoek van Holland (NL).			
(74) Agent: DEN HARTOG, Jeroen, Hendrikus, Joseph; Octrooibureau DSM, P.O. Box 9, NL-6160 MA Geleen (NL).			
(54) Title: RADIATION-CURABLE INK COMPOSITION			
(57) Abstract			
<p>Provided is ribbon assembly having the functional capability of providing break-out of color coded coated glass fibers from said ribbon assembly. The monomers, oligomers and photoinitiator for forming the color coating on the optical glass fibers contained in the ribbon assembly have been selected to provide an average percentage of reacted acrylate unsaturation which provides a level of adhesion between a matrix material and a colored coating that is less than a level of adhesion between the colored coating and the coated optical glass fiber to provide break-out of the color coded optical glass fiber from said ribbon assembly. Also provided are colored coating compositions adapted to form colored coatings suitable for use on optical glass fibers containing in the ribbon assembly.</p>			

*FOR THE PURPOSES OF INFORMATION ONLY*

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece	ML	Mali	TR	Turkey
BG	Bulgaria	HU	Hungary	MN	Mongolia	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MR	Mauritania	UA	Ukraine
BR	Brazil	IL	Israel	MW	Malawi	UG	Uganda
BY	Belarus	IS	Iceland	MX	Mexico	US	United States of America
CA	Canada	IT	Italy	NE	Niger	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NL	Netherlands	VN	Viet Nam
CG	Congo	KE	Kenya	NO	Norway	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NZ	New Zealand	ZW	Zimbabwe
CI	Cote d'Ivoire	KP	Democratic People's Republic of Korea	PL	Poland		
CM	Cameroon	KR	Republic of Korea	PT	Portugal		
CN	China	KZ	Kazakhstan	RO	Romania		
CU	Cuba	LC	Saint Lucia	RU	Russian Federation		
CZ	Czech Republic	LI	Liechtenstein	SD	Sudan		
DE	Germany	LK	Sri Lanka	SE	Sweden		
DK	Denmark	LR	Liberia	SG	Singapore		
EE	Estonia						

RADIATION-CURABLE INK COMPOSITION

5

The invention relates to a radiation curable ink composition, a method for preparing a coated and colored optical glass fiber, a coated and colored optical glass fiber, and a ribbon-assembly comprising  
10 such coated and colored optical glass fibers.

Optical glass fibers are generally coated with two superposed radiation-cured coatings, which together form a primary coating. The coating which is in direct contact with the glass is called the inner  
15 primary coating and the overlaying coating(s) is called the outer primary coating. The inner primary may also be called the primary coating; then, the outer primary coating is called the secondary coating. Both definitions are used interchangeably.

20 The inner primary coating is usually a relatively soft coating providing environmental protection to the glass fiber and resistance, inter alia, to the well-known phenomenon of microbending. Microbending in the coated fiber can lead to attenuation  
25 of the signal transmission capability of the coated fiber and is therefore undesirable. The outer primary coating(s), which is on the exposed surface of the coated fiber, is typically a relatively harder coating designed to provide a desired resistance to physical  
30 handling forces, such as those encountered when the fiber is cabled.

In telecommunications applications of optical fibers, multiple individual strands of coated fiber must be packaged into larger structures such as ribbons and cables to maximize efficiency. However, after ribboning and cabling of fiber, the individual strands of fiber must be readily distinguishable from each other so they can be accurately identified during, for example, installation and repair. Cable geometry and/or color coding can be used to distinguish and identify individual fibers in a complex cable. Although several methods can be used to color code fiber, color coding can be done advantageously with either a thin ink layer (< 10 microns) which is placed over the coated fiber before ribboning and cabling or by using a colored outer primary coating.

Tape-like optical fiber ribbons are prepared by embedding a plurality (e.g., 4 to 12) of individual color coded fibers in a supporting matrix material which, like the inner and outer primary coatings, is also radiation-curable to maximize production speed. The matrix material can encase the color coded optical glass fiber or the matrix material can edge-bond the glass fibers together. Cure of the matrix material occurs during the ribboning stage after the fibers have been color coded by ink. Hence, in a ribbon design, the ink layer resides between the ribbon's matrix material and the fibers' outer primary coating. This means that the ink layer's interfacial characteristics (e.g., surface energy, adhesion) must be carefully controlled to function properly with both matrix material and outer primary coating in the ribbon structure. In particular, the ability of a cured matrix material to be suitably stripped off the ink layer (break-out) is an important technical consideration. Ribbon

break-out is generally carried out by a mechanical force, although chemical softening of the matrix with use of solvents is also known.

Optical fiber color coding can be based on up to  
5 12 or more colors. Although optical fiber inks were originally solvent-based or thermosetting inks, in more recent times, radiation-curable inks have been used to increase the speed of the inking process. In these ink compositions, pigment is dispersed in a radiation-curable  
10 carrier or base composition.

As the demand for coated optical glass fibers has increased, manufacturers must respond by adding more fiber drawing production lines and by attempting to increase the linear line speeds of the existing fiber  
15 drawing production lines. In the latter case, one factor which will determine the upper limit for the line speed will be the curing rate characteristics of the radiation-curable ink composition, for a given radiation source and intensity.

20 If the line speed is increased to the extent that cure rate time requirements of the radiation-curable ink composition are not provided, the radiation-curable ink composition will not have received a sufficient amount of radiation to cause complete cure, or cross-linking, of  
25 the radiation-curable ink composition. The production linear line speed is generally inversely related to the amount of radiation striking the optical glass fiber. That is, as the production line speed is increased the amount of radiation exposure to the radiation-curable ink  
30 composition during the production process will necessarily

decrease for a given radiation source. Incomplete cure of the radiation-curable ink composition is undesirable and must be avoided because then the desired properties of the incompletely cured ink coating may not be achieved and/or the incompletely cured ink coating may retain tackiness (giving problems in subsequent handling) or a malodorous odor may be present, and there may also be an increase in the extractables (undesirable) in the supposedly-cured ink coating.

10 In general, radiation-curable ink coating compositions can cure at a significantly slower rate than radiation-curable outer primary coating compositions. It is believed that the pigments present in ink compositions contribute to the slower cure speed of ink coatings. Thus, 15 there is a need for improving the cure speed of the ink coating.

While the ink composition must have a very fast cure speed to ensure complete cure of the ink coating on the high speed drawing units, the increase in cure 20 speed should not come at the expense of other important properties of the ink coating, such as providing suitable break-out performance. Break-out performance is the ability of the cured ink coating to separate from the matrix material without separating the ink layer from the 25 outer primary coating to provide mid-span access to the individual coated optical glass fibers contained within the ribbon-assembly. Mid-span access is access to the coated optical glass fibers at a portion of the ribbon assembly between the ends of the ribbon assembly.

Therefore, there is a need for a radiation-curable ink composition that exhibits adaptable adhesion properties to provide an adhesion between the outer primary coating and the ink coating that is greater than the adhesion between  
5 the ink coating and the matrix material to provide mid-span access.

In addition, ink compositions should not contain ingredients that can migrate to the surface of the optical glass fiber and cause corrosion. The ink  
10 composition should also not contain ingredients which can cause instability in the protective coatings or matrix material. Ink coatings for optical glass fibers should be color fast for decades, not cause attenuation of the signal transmission, be impervious to cabling gels and  
15 chemicals, and allow sufficient light penetration for fiber core alignment.

Analogous requirements exist for colored outer primary coatings. In particular, these coatings require high cure speed despite the presence of pigments, good  
20 break-out properties, good adhesion to the inner primary coating, and the coating should contain no ingredients that may cause attenuation of light through the glass fiber after prolonged exposure of the ribbon to moist, heat, etc.

25 From the above, it is clear that optical glass fiber technology places many unique demands on radiation-curable colored compositions which more conventional technologies, such as printing inks, do not.

U.S. patent No. 4,629,285 discloses a method

for making an ink coating on a coated optical glass fiber in which a UV curable ink is applied to a coated optical glass fiber. The ink coating is applied in a method that preserves the concentricity of the optical glass fibers.

5 The preferred inks are pigmented semi-opaque UV curable polymeric inks. However, the ink compositions disclosed in this patent do not have a sufficiently fast enough cure speed to be used on modern high speed optical glass fiber drawing and coating towers.

10 Published Japanese Patent Application No. H1-152405 discloses a radiation-curable ink composition containing an organic polysiloxane compound. The polysiloxane compound provides the ink coating with the ability to separate more easily from the matrix material  
15 in a ribbon assembly.

Published Japanese Patent Application No. 64-22976 discloses radiation-curable ink compositions containing specific radiation-curable oligomers. The ink composition provides an ink coating having adhesion to the  
20 outer primary coating which is separable from the matrix material in a ribbon assembly.

Patent application EP-A-614099 describes the use of a release agent such as a silicon oil or a fluororesin between the bundling layer and the coloring layer. In  
25 particular, when substantial amounts of silicone resins are used, incompatibility in the liquid and resultant imperfections in the cured matrix composition may result, which causes attenuation of light.

Usually ink compositions must be cured in an



inert atmosphere, i.e. in the absence of oxygen.

Providing inert atmospheres on optical glass fiber drawing towers is expensive. Thus, a radiation-curable ink composition which exhibits a high cure speed in the  
5 presence of some oxygen like in an air atmosphere would provide significant advantages over ink compositions that must be cured in an inert atmosphere.

An objective of the present invention is to provide ribbon assemblies having suitable break-out  
10 performance, without requiring the use of substantial amounts of a silicone agent in the ink composition.

Another objective of the present invention is to provide radiation-curable ink compositions which are adapted to provide cured ink coatings having greater  
15 adhesion to the outer primary coating than to a matrix material, to provide the ribbon assembly with the capability of break-out of the individual coated optical glass fibers.

A further objective of the present invention  
20 is to provide high speed radiation-curable ink compositions which provide enhanced cure speed in the presence of air.

Another objective of the present invention is to provide an ink composition which exhibits enhanced  
25 adhesion to the outer primary coating when suitably cured.

Other objectives of the present invention are to provide an optical glass fiber coated with the ink composition and a ribbon assembly containing at least one of the coated optical glass fibers.

30 The above objectives and other objectives can

be obtained by the novel ribbon assemblies according to the present invention. Provided is a novel ribbon assembly having the functional capability of providing break-out of color coded optical glass fibers from the ribbon assembly.

5 The ribbon assembly comprises a plurality of coated optical glass fibers having an ink or colored secondary coating on at least one of the coated optical glass fibers; and a matrix material binding the plurality of coated optical fibers together. The colored coating is  
10 formed from a radiation curable coating composition comprising a radiation-curable carrier system containing a mixture of radiation-curable monomers and oligomers and at least one photoinitiator; and a pigment dispersed in the radiation-curable carrier system. The monomers, oligomers  
15 and photoinitiator have been selected to provide an average percentage of reacted acrylate unsaturation which provides a level of adhesion between the matrix material and the colored coating that is less than a level of adhesion between the colored coating and the coated  
20 optical glass fiber to provide break-out of the colored coated optical glass fiber from the ribbon assembly when the colored coating composition is cured by exposure to a suitable ultraviolet radiation dose. In a preferred embodiment, the suitable dose is a dose of about 0.125  
25 joules per square centimeter. The invention is in particular useful for ink coatings that are applied on a coated optical glass fiber, and that are adjacent to an outer primary coating.

Also provided is a novel assembly having the

functional capability of providing break-out of the individual coated optical glass fibers. The ribbon assembly comprises a plurality of coated optical glass fibers; and a matrix material which binds the plurality of coated optical glass fibers together. At least one of the coated optical glass fibers comprises an optical glass fiber; an inner primary coating adjacent to a surface of the optical glass fiber; an outer primary coating adjacent to a surface of the outer primary coating. The ink coating is formed from a radiation-curable ink coating composition containing a monomer selected to be adsorbable into the outer primary coating to a degree which when suitably cured provides a level of adhesion between the ink coating and the outer primary coating that is greater than a level of adhesion between the ink coating and the matrix material.

Also provided are novel radiation-curable ink coating compositions which are capable of providing ink coatings suitable for use in ribbon assemblies when the property of break-out is desired.

Also provided by the present invention is a radiation-curable ink coating composition comprising

- a) an oligomer
- b) a reactive diluent
- c) a homolytic photoinitiator
- d) a pigment, and
- e) additives

wherein the composition comprises more than about 1 wt.% homolytic photoinitiator in combination with a benzophenone-type compound.

This composition if suitably formulated, using the constituents a-e, can also be used as a colored outer primary coating.

Unexpectedly, this use of a benzophenone-type compound - if suitably cured - results in a system having a satisfactory adhesion to an outer primary coating and good break-out from the matrix material.

In DE-A-4007519, it is described to use photoinitiators in the curing of UV curable ink compositions on optical fibers. However, this reference does not teach to use the combination of a substantial amount of homolytic types of photoinitiators in combination with substantial amounts of benzophenone.

The radiation-curable ink compositions comprise two functional components: a pigment system which functions to impart color and a radiation-curable carrier system which functions to allow the pigment system into a coherent, high-quality film after radiation-cure. Typically, a carrier system will be mixed with a pigment system to form the radiation-curable ink.

Ink coatings are usually about 3 to about 10 microns thick, and should be concentric to prevent attenuation of the signal transmission. The ink coating also generally has a  $T_g$  of at least about 30°C, more preferably at least about 50°C.

Colored outer primary coatings, generally are 10-30  $\mu\text{m}$  thick, and are described e.g. in EP-B-473643.

Radiation-curable carrier systems which are suitable for forming the present ink composition contain one or more radiation-curable oligomers and monomers having at least one functional group capable of polymerization when exposed to actinic radiation. Suitable

radiation-curable oligomers or monomers are now well known and within the skill of the art.

The coated optical glass fibres each have an ink coating for identifying the individual fibers. The level of adhesion between the ink coating and the matrix material has been adjusted to be less than the level of adhesion between the ink coating and the secondary coating on the optical glass fiber, which provides the functional capability of providing break-out of the individual coated optical glass fibers. The level of adhesion between the ink coating and the secondary coating and the level of adhesion between the ink coating and the matrix material can be adjusted to suitable levels according to various embodiments of the present invention by the following:

- (1) decreasing the adhesion between the ink coating and the matrix material of the ribbon assembly by utilizing monomers, oligomers and a photoinitiator in the ink coating composition that provide an increase in the percent reacted acrylate unsaturation ("%RAU"), when exposed to about 0.125 J/cm<sup>2</sup> UV radiation; and/or
- (2) increasing the adhesion between the ink coating and the outer primary coating of the ribbon assembly by including a monomer in the ink coating composition which is adsorbable into the outer primary coating to a greater degree.

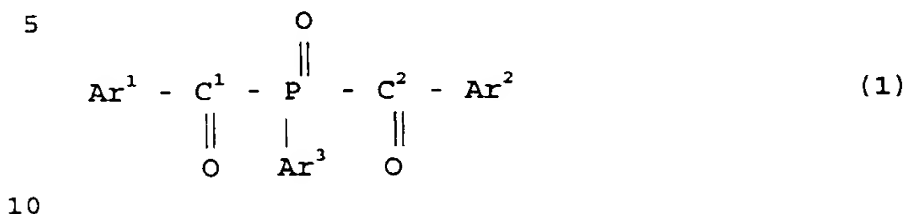
The conventional ink compositions can become the improved ink composition according to the present invention by selecting monomers, oligomers and a

photoinitiator which provide a %RAU", when exposed to about 0.125 J/cm<sup>2</sup> UV radiation, such that the level of adhesion between the ink coating and the matrix material is less than the level of adhesion between the ink coating and the outer primary coating. Preferably, the average %RAU is at least 70%, more preferably at least about 75%, and most preferably at least about 80%, when cured in the presence of an oxygen containing gaseous atmosphere, like air. Preferably, the average %RAU is at least 75%, more preferably at least about 80%, and most preferably at least about 85%, when cured in an inert (e.g. nitrogen) atmosphere. The average %RAU should be based on the %RAU of at least four different color ink coating compositions, each having the same radiation-curable carrier system. Preferably, the %RAU is based on at least 6, more preferably at least 12, different color ink coating compositions.

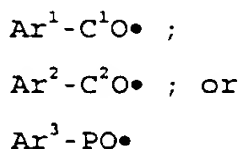
Without being bound by any theory, it is believed that the fewer the amount of unreacted acrylate present on the ink coating, the fewer the number of sites for cross-linking between the matrix material and the ink coating. The fewer the number of cross-linking sites, the lower the level of adhesion between the ink coating and the matrix material. As the %RAU increases, the amount of unreacted acrylate decreases. Thus, the higher %RAU the lower the adhesion between the ink coating and the matrix material.

The %RAU can adjusted to a suitable level by utilizing an ink cure speed enhancing photoinitiator. The

ink cure speed enhancing photoinitiator preferably comprises a free-radical generating photoinitiator represented by the following formula (1):



Where: Ar represents a carbon containing compound having at least one aromatic functional group, wherein "P" is bonded directly to an aromatic functional group present in Ar<sup>3</sup>, C<sup>1</sup> is bonded directly to an aromatic functional group present in Ar<sup>1</sup>, and C<sup>2</sup> is bonded directly to an aromatic functional group present in Ar<sup>2</sup>. At least one of the carbon containing compounds "Ar" has a molecular weight and molecular structure that is suitable for forming at least one of the following free-radicals:

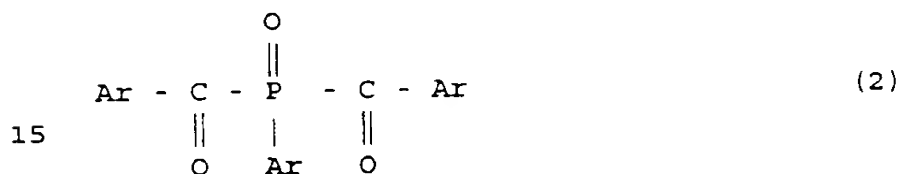


Preferably, all three carbon containing compounds "Ar" have a molecular weight and molecular structure that is suitable for forming the above free-radicals. For example, the carbon containing compounds can have from about 5 to about 15 carbon atoms. Suitable examples of the carbon containing compounds include a furane ring or a benzene ring.

30

One or more of the hydrogens present on the aromatic ring can be substituted, for example, with alkyl and/or alkoxy groups. Examples of suitable alkyl substituents include methylene, ethylene, butylene and propylene groups. Examples of suitable alkoxy substituents include methoxylate, ethoxylate, butoxylate and propoxylate groups.

A preferred cure speed enhancing photoinitiator includes one represented by the following formula (2):



wherein Ar is a phenyl group, optionally substituted with one to three alkyl groups having 1-4 carbon atoms.

The radiation-curable ink composition can also contain other free-radical generating photoinitiators in combination with the ink cure speed enhancing photoinitiator. Examples of suitable free radical-type photoinitiators (also called Norrish type I photoinitiators) include, but are not limited to, the following:

- 2,4,6 trimethylbenzoyl diphenylphosphine-oxide;
- 1-hydroxycyclohexylphenyl ketone;
- 2-benzyl-2-dimethylamino-1-(4-morpholinophenyl)-butan-1-



- one;  
2,2-dimethoxy-2-phenylacetophenone;  
2-methyl-1-[4-(methylthio)phenyl]-2-(4-morpholinyl)-1-propanone;  
5 2-hydroxy-2-methyl-1-phenyl propan-1-one;  
4-(2-hydroxyethoxy)phenyl-2-hydroxy-2-propyl ketone  
dimethoxyphenylacetophenone;  
1-(4-isopropylphenyl)-2-hydroxy-2-methylpropan-1-one;  
1-(4-dodecyl-phenyl)-2-hydroxy-2-methylpropan-1-one;  
10 4-(2-hydroxyethoxy)phenyl-2-(2-hydroxy-2-propyl)-ketone;  
diethoxyphenyl acetophenone;  
a mixture of (2,6-dimethoxy benzoyl)-2,4,4  
trimethylpentylphosphineoxide and 2-hydroxy-2-methyl-1-phenyl-propan-1-one;  
15 benzophenone;  
1-propanone, 2-methyl-1-[4-(methylthio)phenyl]-2-(4-morpholinyl); and  
mixtures of these.

- Preferably, the radiation-curable ink  
20 composition contains a mixture of benzophenone and 2-methyl-1-[4-(methylthio)phenyl]-2-(4-morpholinyl)-1-propanone.

- Preferably, the ink cure speed enhancing photoinitiator is present in an amount which provides the  
25 desired %RAU. In general, the greater the amount of ink cure speed enhancing photoinitiator, the higher the %RAU. Suitable amounts of the ink cure speed enhancing photoinitiator are from about 1 to about 25 weight%, preferably from about 1.5 to about 20 weight%, and most

preferably from about 4 to about 15 weight%, based on the total weight of the ink composition. In general, if other photoinitiators are present in the ink composition in combination with the ink cure speed enhancing  
5 photoinitiator, the ink cure speed enhancing photoinitiator can be used in lesser amounts to provide the desired cure speed.

As the amount of radiation that a radiation-curable ink composition is exposed to is increased, the  
10 amount of a specific physical or performance property of the cured ink coating (measured as a percentage of the fully attainable value for the specific ink composition) correspondingly increases. This increase continues until the maximum attainable value of the measured physical or  
15 performance property is achieved. The maximum attainable value of a physical or performance property cannot be exceeded by further exposure to radiation. Examples of physical or performance properties are cross-link density as measured using MEK, modulus, glass transition  
20 temperature, hardness, surface adhesion, and remaining extractables. Cross-link density as measured using MEK is used herein by way of example.

Once the measured cross-link density reaches the maximum attainable value, further exposure to  
25 radiation does not result in an increase in the cross-link density. For purposes of comparing cure speeds among different radiation-curable ink compositions, the term "cure speed" is used to represent the radiation dose which provides a cross-link density such that the MEK value is a

predetermined set number rubs at a thickness of 20  
microns. The lower the radiation dose required to attain  
an MEK value of the predetermined set number rubs, the  
faster the cure speed. If desired, other physical  
5 properties can be used to compare the cure speeds of  
different radiation-curable compositions, however, the MEK  
value is preferred.

The cure speed enhancing photoinitiator can be  
present in an amount which provides the radiation-curable  
10 ink composition containing at least one pigment that  
absorbs light in a visible wavelength with a cure speed  
such that a MEK value of at least 25 rubs is achieved  
using an irradiation of about  $0.125 \text{ J/cm}^2$  or less at a  
thickness of 20 microns in an air atmosphere. Preferably,  
15 the cure speed enhancing photoinitiator is present in an  
amount which provides the radiation-curable ink  
composition containing at least one pigment that absorbs  
light in a visible wavelength with a cure speed such that  
a MEK value of at least about 100 rubs, more preferably at  
20 least about 200 rubs, is achieved using an irradiation of  
about  $0.125 \text{ J/cm}^2$  or less at a thickness of 20 microns in  
an air atmosphere.

Ink coatings are usually about 3 to about 10  
microns thick, and should be concentric to prevent  
25 attenuation of the signal transmission. The ink coating  
also generally has a  $T_g$  of at least about  $30^\circ\text{C}$ , more  
preferably at least about  $50^\circ\text{C}$ . One of ordinary skill in  
the art of formulating radiation-curable ink compositions  
knows how to adjust the radiation-curable composition to

provide the desired properties of the cured coating. Thus, radiation-curable compositions which are usually used for forming outer primary coating compositions can be reformulated and utilized as the radiation-curable carrier system in the ink composition according to the present invention.

The colored secondary coatings of the present invention can be formulated by mixing a suitable amount of pigment (generally 1-10 wt.%) to the carrier composition. These colored secondary coatings preferably are formulated to achieve the %RAU and MEK double rubs values as defined above.

Examples of suitable radiation-curable compositions which may be reformulated variously include those which are disclosed in U.S. patent numbers 4,624,994; 4,682,851; 4,782,129; 4,794,133; 4,806,574; 4,849,462; 5,219,896; and 5,336,563, all of which are incorporated herein by reference.

Radiation-curable carrier systems which are suitable for forming the present ink composition contain one or more radiation-curable oligomers or monomers having at least one functional group capable of polymerization when exposed to actinic radiation. Suitable radiation-curable oligomers or monomers are now well known and within the skill of the art.

Commonly, the radiation-curable functionality used is ethylenic unsaturation, which can be polymerized through radical polymerization or cationic polymerization. Specific examples of suitable ethylenic unsaturation are

groups containing acrylate, methacrylate, styrene, vinyl ether, vinyl ester, N-substituted acrylamide, N-vinyl amide, maleate esters, and fumarate esters.

Preferably, the ethylenic unsaturation is provided by a group containing acrylate, methacrylate, or styrene functionality.

Preferably, at least about 80 mole %, more preferably, at least about 90 mole %, and most preferably substantially all of the radiation-curable functional groups present in the oligomer are acrylate or methacrylate.

A suitable radiation-curable ink composition essentially consists of from about 1 to about 80 weight % of at least one radiation-curable oligomer (a). Preferred amounts of the radiation-curable oligomer include from about 20 to about 70 % by weight, based on the total weight of the ink composition.

A mixture of mono-, di-, tri-, tetra-, and higher functionalized oligomers can be used to achieve the desired balance of properties, wherein the functionalization refers to the number of radiation-curable functional groups present in the oligomer.

The oligomers usually comprise a carbon-containing backbone structure to which the radiation-curable functional group(s) are bound. Examples of suitable carbon-containing backbones include polyethers, polyolefins, polyesters, polyamides, and polycarbonates. The size of the carbon-containing backbone can be selected to provide the desired molecular weight. The number

average molecular weight of the oligomer is usually between about 500 to about 10,000, preferably between about 500 to about 7,000, and most preferably between about 1,000 to about 5,000.

5                   For example, the carbon-containing backbone of the oligomer can comprise aromatic groups and ring-opened epoxy groups or alkoxy groups. The oligomer can be represented by, for example:

10                   R-Ar-R; or  
                    R-L-Ar-L-R

                    where R is a radiation-curable functional group,

15                   Ar is an aromatic group containing moiety, and L is a linking group.

                    Examples of suitable linking groups include alkoxy or ring opened epoxy such as ethoxy, propoxy, butoxy, and repeat units thereof. L can also be a urethane  
20   or urea linking group.

                    The aromatic groups can be, for example, derived from bisphenol units, such as bisphenol A. A preferred oligomer is a diglycidyl ether derivative of bisphenol A to which acrylate functional groups have been  
25   bound. A commercially available example of such an oligomer is Ebecryl 3700 (UCB) or CN-120 (Sartomer), the latter having a molecular weight of about 1300, and when cured has a Tg of about 65°C.

                    Another example of a preferred oligomer is a

trifunctional polyether or polyester having a molecular weight of about 500 to about 5000. A preferred example of a trifunctional oligomer is the commercially available polyurethane triacrylate Ebecryl 264, which has a  
5 molecular weight of about 2000 and when cured a Tg of about 42°C.

The radiation-curable carrier systems may also contain a reactive diluent (b) which is used to adjust the viscosity. The reactive diluent can be a low viscosity  
10 monomer containing having at least one functional group capable of polymerization when exposed to actinic radiation. This functional group may be of the same nature as that used in the radiation-curable monomer or oligomer. Preferably, the functional group present in the reactive  
15 diluent is capable of copolymerizing with the radiation-curable functional group present on the radiation-curable monomer or oligomer.

A suitable radiation-curable ink composition essentially consists of from about 1 to about 80 weight %  
20 of at least one radiation-curable diluent. Preferred amounts of the radiation-curable diluent include from about 5 to about 60 % by weight, more preferably from about 10 to about 50 % by weight, based on the total weight of the ink composition.

25 Preferably, compound b) is a reactive diluent or a mixture thereof. Generally, each reactive diluent has a molecular weight of less than about 550 and a viscosity of less than about 500 mPa.s

For example, the reactive diluent can be a  
30 monomer or mixture of monomers having an acrylate or vinyl

ether functionality and a C4-C20 alkyl or polyether moiety.

Particular examples of such reactive diluents include: hexylacrylate, 2-ethylhexylacrylate, isobornylacrylate, decylacrylate, laurylacrylate, 5 stearylacrylate, 2-ethoxyethoxy-ethylacrylate, laurylvinyether, 2-ethylhexylvinyl ether, N-vinyl formamide, isodecyl acrylate, isooctyl acrylate, N-vinyl caprolactam, N-vinylpyrrolidone, and the like.

10 Another type of reactive diluent that can be used is a compound having an aromatic group. Particular examples of reactive diluents having an aromatic group include: ethyleneglycolphenylether-acrylate, polyethyleneglycolphenylether-acrylate, 15 polypropyleneglycolphenylether-acrylate, and alkyl-substituted phenyl derivatives of the above monomers, such as polyethyleneglycolnonylphenyletheracrylate.

The reactive diluent can also comprise a diluent having two or more functional groups capable of 20 polymerization. Particular examples of such monomers include:

C<sub>2</sub>-C<sub>18</sub> hydrocarbon-dioldiacrylates,  
C<sub>4</sub>-C<sub>18</sub> hydrocarbondivinylethers,  
C<sub>3</sub>-C<sub>18</sub> hydrocarbon triacrylates, and the polyether  
25 analogues thereof, and the like, such as  
1,6-hexanedioldiacrylate,  
trimethylolpropanetri-acrylate,  
hexanedioldivinylether,  
triethylene-glycoldiacrylate,  
30 pentaerythritol-triacrylate,  
ethoxylated bisphenol-A diacrylate, and  
tripropyleneglycol diacrylate.



Preferably, alkoxyated aliphatic polyacrylates are used, such as ethoxylated hexanedioldiacrylate, propoxylated glyceryl triacrylate or propoxylated trimethylolpropanetriacrylate.

5           At least one of the photoinitiators c) used in the ink coating composition of the present invention is a homolytic fragmentation photoinitiator (also called a Norrish Type I photoinitiator) which operates by intramolecular bond cleavage.

10           A suitable radiation-curable ink composition essentially consists of from about 1 to about 20 weight% of a homolytic photoinitiator. Preferred amounts of the homolytic photoinitiator are from greater than 3 to about 15% by weight, more preferably from about 4 to about 12%  
15 by weight.

Examples of free radical-type photoinitiators include, but are not limited to, the photoinitiators that are described above.

As a pigment is present in the composition  
20 according to the invention, it is preferred (also for colored secondary coating compositions) to use as photoinitiator an acyl phosphine oxide photoinitiator, more specifically a benzoyl diaryl phosphine oxide photoinitiator. Examples of suitable benzoyl diaryl  
25 phosphine oxide photoinitiators include:  
2,4,6-trimethylbenzoyldiphenyl-phosphine oxide (Lucirin TPO by BASF), and bis(2,6-dimethoxybenzoyl)-2,4,4-trimethylpentyl-phosphine oxide (Irgacure 1700 by Ciba Geigy).

30           For an optimum cure speed in the presence of pigment, it is advantageous to combine an acyl phosphine

oxide photoinitiator with one or more other photoinitiators, such as hydroxy-cyclohexylphenyl-ketone.

Any inorganic and organic pigment (d) that is suitable for making radiation-curable ink compositions can  
5 be used in the present invention. However, because white pigments usually do not absorb significant amounts of the radiation used to cure the ink composition, white ink compositions do not usually require the use of the ink cure speed enhancing photoinitiator according to the  
10 present invention. Therefore, the preferred pigments are pigments that absorb light of a visible wave length, i.e. any color except pure white. The use of the term "pigment" refers to both inorganic and organic pigments.

Preferably, the pigment used in the ink  
15 coating composition of the present invention is an organic pigment. The pigment can be present in the ink composition in an amount that provides coloration that is visible without magnification to facilitate identification of the individual colored optical glass fiber.

20 Ribbon assemblies utilizing 12 or less coated optical glass fibers require only 12 colors to adequately distinguish each of the coated optical fibers from one another. However, in larger ribbon assemblies, more than 12 colors may be utilized to adequately distinguish the  
25 coated optical glass fibers from one another. Examples of twelve colors normally used for making ribbon assemblies include: black, white, yellow, blue, red, green, orange, brown, pink, aqua, violet, and gray.

Preferably, the pigment has a mean particle size of not more than about 1  $\mu\text{m}$ . The particle size of the commercial pigments can be lowered by milling if necessary.

5           A specific example of a suitable black pigment includes carbon black.

A specific example of a suitable white pigment includes titanium dioxide.

Specific examples of suitable yellow pigments  
10 include diarylide yellow and diazo based pigments.

Specific examples of suitable blue pigments include phthalocyanine blue, basic dye pigments, and phthalocyanines.

Specific examples of suitable red pigments  
15 include anthraquinone (red), naphthole red, monoazo based pigments, quinacridone pigments, anthraquinone, and perylenes.

Specific examples of suitable green pigments include phthalocyanine green and nitroso based pigments.

20           Specific examples of suitable orange pigments include monoazo and diazo based pigments, quinacridone pigments, anthraquinones and perylenes.

Specific examples of suitable violet pigments include quinacrinode violet, basic dye pigments and  
25 carbazole dioxazine based pigments.

Suitable aqua, brown, gray, and pink colors can easily be formulated by combining several pigments. One skilled in the art is able to form any color as desired by combining different pigments.

The pigment can be present in the ink composition in an amount that provides coloration that is visible without magnification to facilitate identification of the individual colored optical glass fiber. The amount of the pigment should not be so great as to significantly reduce the cure speed of the ink composition or result in other undesirable affects. Examples of suitable amounts of pigment have been found to be higher than about 1-25 weight %. Generally, the amount is less than 25 wt.%, preferably less than about 20 weight %, more preferably less than about 10 weight %, based on the total weight of the ink composition.

Preferred amounts of each pigment are from about 0.5 to about 10 % by weight, more preferably from about 0.5 to about 5 % by weight. In colored secondary coatings, generally lower amounts of pigments are sufficient to achieve good coloring.

Other additives which can be used in the radiation-curable carrier system include, but are not limited to, lubricants, wetting agents, antioxidants and stabilizers. The selection and use of such additives is within the skill of the art.

Coated optical fibers are often used in ribbon assemblies. Because of the versatility of the presently invented ink coating composition, this composition is very well suited for use on coated optical glass fibers in ribbon assemblies. If necessary, a release agent can be added to the ink coating to allow easy access to the individual fibers by separating the matrix material from

the ink coating, usually called break-out. However, preferably, no substantial amount of release agents is used. Suitable release agents include silicones, silicone acrylates, fluoro-carbon oils or resins and the like. If present, the ink coating composition for coating optical fibers used in ribbon assemblies comprises about 0.1 to about 20 wt.%, more preferably about .1 to about 10 wt. % of a suitable release agent, based on the total weight of the ink composition.

Useful additives e) of the ink coating are a small amount of lubricant to allow even better access to the individual fibers in separating the matrix material from the ink coating, usually called break-out. Suitable lubricants include silicones, fluoro-carbon oils or resins and the like. Reactive release agents such as silicone acrylates appear to have no further effect. Preferably, the ink coating composition for coating optical fibers used in ribbon assemblies comprises about 0.01 to about 5 wt % more preferably about 0.1 to about 3 wt% of a suitable lubricant, based on the total weight of the ink composition.

Preferably, a silicon oil is used. Another lubricant compound can be present to a lesser extent.

In a preferred embodiment of the ink coating composition of the present invention comprises an effective amount of a benzophenone-type compound to achieve a better break-out of the matrix material from the coated and colored optical fiber. A suitable radiation-cured ink composition of this embodiment comprises more than about 2 weight % of a benzophenone-type compound.

Preferred amounts of the benzophenone-type compound are more than about 3 % by weight, and more preferably more than 3.5 % by weight, based on the total weight of the ink composition. The amount generally will  
5 be less than about 10 % by weight as use of more than about 10 % by weight of the benzophenone-type compound creates no particular advantage, and higher amounts are not recommended from economical point of view. Preferably, the ink composition comprises less than 8 wt.% of  
10 benzophenone-type compound.

Suitable benzophenone-type compounds are organic compounds with a molecular weight between 170 and 500, which consists essentially of a substituted benzophenone group. Suitable substituents are alkyl groups, acryl  
15 groups, aromatic groups, halogens, and the like. Suitable benzophenone-type compounds include benzophenone, chlorobenzophenone, methyl-o-benzoyl benzoate, 4-benzoyl-4'-methyldiphenylsulphide, acrylated benzophenone, 4-phenylbenzophenone, 3,3'-dimethyl-4-methoxybenzophenone,  
20 4,4'-dimethylamino-benzophenone, and the like. Preferably, this benzo-phenone-type compound is not a ring-bonded benzophenone. Ring-bonded benzophenones such as thioxanthone or derivatives thereof, e.g. 2,4-diethyl- or 9-isopropyl-thioxanthone, appear to have little effect on  
25 the improvement of break-out properties.

The ink composition according to the present invention preferably comprises none, or a minor amount of amine compound, which would act as a hydrogen abstraction co-initiator for the benzophenone type compound.

30 Generally, less than 0,5 wt.% and preferably less than 0,1 wt.% of amine type hydrogen abstraction compound would be present in the composition of the

present invention. Nevertheless, morpholino-type sensitizers can be present in amounts up to 4 wt.% but preferably less than 3 wt.%.

Based on the above, a suitable radiation-  
5 curable ink composition can be formulated from a composition containing:

from about 1 to about 20 weight % of at least one pigment that absorbs light of a visible wavelength;

from about 1 to about 25 weight % of at least  
10 one photoinitiator; and

from about 55 to about 98% of a radiation-  
curable carrier system containing at least radiation-  
curable monomer or oligomer, based on the total weight of  
the ink composition.

15 A preferred ink composition can be formulated from a composition containing:

from about 1 to about 20 weight % of at least one pigment which absorbs light of a visible wavelength;

from about 1 to about 80 weight % of at least  
20 one radiation-curable oligomer;

from about 1 to about 80 weight % of at least one radiation-curable diluent monomer; and

from about 1 to about 20 weight % of at least one ink cure speed photoinitiator, based on the total  
25 weight % of the ink composition.

Preferred amounts of the ink cure speed enhancing photoinitiator are from about 1.5 to about 20 weight %, more preferably from about 4 to about 15 weight %.

Preferred amounts of the radiation-curable oligomer include from about 10 to about 70% by weight, more preferably, about 20 to about 60% by weight, based on the total weight of the ink composition.

5 Preferred amounts of the radiation-curable diluent monomer include from about 10 to about 70% by weight, more preferably, about 20 to about 60% by weight, based on the total weight of the ink composition.

Preferably, the ink composition contains other  
10 photoinitiators in an amount of about 1 to about 20% by weight, more preferably about 1 to about 10% by weight, based on the total weight of the ink composition.

Radiation-cure of optical fiber inks can be executed with radiation sources which have characteristic  
15 emission outputs which will vary depending on the radiation source. Exemplary radiation sources can be obtained from, for example, Fusion UV Systems Inc. or Iwasaki Denki Co. For example, so-called "D-lamps" and "H-lamps" can be used as a radiation source, wherein the D  
20 lamp is more rich in longer wavelength ultraviolet light emissions than the H lamp. A typical ultraviolet radiation source (e.g., medium pressure arc lamp) used in industrial production often has major emission lines near the 260,  
300, 313, and 366 nm ranges, or more generally at about  
25 250-270 nm, at about 290-320 nm, and at about 360-380 nm. In addition, there can be a line at about 390-410 nm. The characteristic bulb output used in the present invention can be measured by conventional methods or obtained from the supplier of the radiation source. Preferably, the ink  
30 composition of the present invention is cured by irradiation with both an H and a D lamp.



The colored coating compositions of the present invention preferably are cured with sufficient energy to have less than 15% unreacted acrylate unsaturation. Suitable irradiation energy values are 0.05-2 J/cm<sup>2</sup>,  
5 preferably 0.1-1.5 J/cm<sup>2</sup>. More in particular, values below 0.5 J/cm<sup>2</sup> are particular preferred.

The present invention also provides an ink composition having enhanced adhesion to the outer primary coating when suitably cured. It has been found that  
10 surprisingly the adhesion of the ink coating to the outer primary coating can be approximated by how well a monomer present in the ink composition adsorbs in the outer primary coating. In general, the greater the adsorption of the monomer into the outer primary coating, the greater  
15 the adhesion of the cured ink coating to the outer primary coating.

If the ink coating separates from the outer primary coating during mid-span access to the individual optical glass fibers, the identification of the individual  
20 optical glass fibers can be difficult or even unattainable. Using the present invention, the adhesion of the ink coating to the outer primary coating can be easily adjusted to provide an ink coating having greater adhesion to the outer primary coating than to the matrix material  
25 to provide a ribbon assembly that is capable of providing mid-span access to the individual optical glass fibers while avoiding undesirable delamination of the ink coating from the outer primary coating during mid-span access.

Preferably, the monomer present in the ink composition exhibits an Outer Primary Adsorption Index of at least about 5, preferably at least about 7, and most preferably at least about 10.

5           The adsorption index of the monomer can be determined without undue experimentation by first preparing 75 micron thick drawdown of the outer primary coating to be coated by the ink composition. The drawdown is then suitably cured by exposure to radiation and then  
10 cut into 2 inch by 2 inch sample squares. The sample square is then submerged in the monomer present in the desired ink coating for 30 seconds under atmospheric pressure and room temperature (25°C). The amount of weight gain in the sample expressed as a percentage of the  
15 original weight of the sample is used to determine the outer primary adsorption index as follows.

Outer Primary Adsorption Index:

	1	=	.1% weight gain
	2	=	.2% weight gain
20	3	=	.3% weight gain
	4	=	.4% weight gain
	5	=	.5% weight gain
	6	=	.6% weight gain
	7	=	.7% weight gain
25	8	=	.8% weight gain
	9	=	.9% weight gain
	10	=	1% weight gain

Thus, for an adsorption index of 5 the sample gained about .5% in weight after being submerged in the

monomer for 30 seconds.

The amount of the monomer can be selected to provide the desired level of adhesion between the outer primary coating and the ink coating. In general, the greater the amount of a monomer having an adsorption index of at least about 5, the greater the adhesion between the outer primary coating and the ink coating. Suitable examples of such a monomer are from about 1 to about 20 wt. %, and preferably from about 1 to about 10 wt.%, based on the total weight of the ink composition.

In producing a coated and colored optical fiber, a liquid coating composition is applied to a substrate and subsequently cured. The optical glass fibers are generally coated with two superposed radiation-cured coatings, which together form a primary coating. The inner primary coating is in direct contact with the glass and the outer primary coating is adjacent to the surface of the inner primary coating. The ink coating composition according to the present invention can be formulated to provide an ink coating having a good adhesion to the outer primary coating.

It is also possible to use a colored outer primary coating, which precludes the necessity of using an extra ink layer. The outer primary coating should adhere well to the inner primary coating, and the matrix material should show good break-out properties with respect to the colored secondary coating, which can be achieved using the ink coating of the present invention as the colored secondary coating.

The above embodiments can be used in combination to provide an improved radiation-curable ink

composition which exhibits the combination of properties of:

- (i) when suitably cured provides the ribbon assembly with the functional capability of providing break-out without delaminating the ink or colored coating from the outer resp. inner primary coating;
- (ii) when suitably cured provides sufficient adhesion between the matrix material and the ink coating to resist delamination; and
- (iii) exhibits an enhanced cure-speed in the presence of an oxygen containing atmosphere such that the colored coating can be formed at high speed without the need for providing an inert atmosphere.

The ink coating composition can be applied to the coated optical glass and cured using any suitable method. An example of a suitable method is disclosed in U.S. patent No. 4,629,285, the complete disclosure of which is incorporated herein by reference. The ink composition can also be applied in a manner similar to the application of the outer primary coating on an optical glass fiber drawing and coating tower.

Because of the versatility of the presently invented ink coating composition, this composition is very well suited for use on coated optical glass fibers in ribbon assemblies. Multiple individual strands of coated fiber are packaged into larger structures such as ribbons and cables to maximize efficiency. One skilled in the art will easily be able to use the disclosure provided herein to prepare a novel ribbon assembly containing at least one

of the improved ink coated optical glass fibers for the desired applications. The novel ribbon assembly made according to this invention can be used in telecommunication systems. Such telecommunication systems typically include ribbon assemblies containing optical glass fibers, transmitters, receivers, and switches. The ribbon assembly containing the coated optical glass fibers are the fundamental connecting units of telecommunication systems. The ribbon assembly can be buried under ground or water for long distance connections, such as between cities. The ribbon assembly can also be used to connect directly to residential homes.

The novel ribbon assembly made according to this invention can also be used in cable television systems.

The ink compositions according to the present invention are surprisingly suitable for formulating radiation-curable colored coating compositions for forming protective and/or decorative coatings having a thickness greater than about 10 microns, and up to about 50 microns. While ink coatings on optical glass fibers usually have a thickness of about 3 to about 10 microns, the cure speed of the ink compositions according to the present invention have been described above using a thickness of 20 microns. Thus, at the thinner thicknesses usually used for forming an ink coating on an optical glass fiber, such as from about 3 to about 10 microns, the MEK rub value will be significantly greater than the MEK rub value measured at a 20 micron thickness. In general, as the thickness of the

ink coating is increased, the cure speed decreases.

Thicker colored coatings tend to have a decreased concentration of pigment, based on the total weight of the colored coating, compared to ink coating.

- 5 Because the colored coating is applied in at a thickness greater than ink coatings, a lower concentration of pigment is required to obtain the desired color.

The colored coating composition exhibits an enhanced cure speed and therefore is commercially feasible  
10 for use on high speed production lines, such as for appliances. The colored coating composition is also suitable for application to aircraft and automobile parts.

The invention will be further explained by way of the following examples, without being limited thereto.

15

Example I

A radiation-curable base composition was first formed by combining the components shown in Table 1.

Table 1

Component	Amount (% by weight of total composition)
Ethoxy Diacrylate Monomer <sup>1</sup>	42.85
Aliphatic Urethane Diacrylate Oligomer <sup>2</sup>	25.25
Pentaerythritol Tetra-acrylate	12.55
1,6-Hexanediol Diacrylate	1.68
Isobornyl Acrylate	3.88
Phenoxy Ethyl Acrylate	3.88
Butylhydroxy Toluene	0.52
Benzophenone	8.33
2-Methyl-1-(4-(Methylthio)-phenyl)-2-(4-Morpholinyl)-1-Propanone	1.04

<sup>1</sup> CN120, (Sartomer)

5 <sup>2</sup> Ebecryl 264, (Radcure)

96% of this base composition was then combined with the 4% of CGI 819 (Ciba Geigy) to form a radiation-curable composition. 88 wt.% of the radiation-curable composition was combined with 9 wt.% of blue, and 3 wt.% of white pigment to form a radiation-curable ink composition.

10

A 20 micron thick drawdown of the ink

compositions was formed on a mylar film and then exposed to 0.1 J/cm<sup>2</sup> UV light to form a sample film.

The following properties of the sample film was tested:

- 5                   (1) MEK rub;  
                  (2) Unreacted Coating; and  
                  (3) Undercut.

The MEK rub test represents the degree of cross-linking that occurred in the sample. In general, the  
10 greater the number of rubs required to disintegrate the sample, the greater the degree of cross-linking, and the faster the ink composition cured.

The unreacted coating test was a visible test for the presence of uncured coating on the sample. The  
15 presence of uncured coating signifies that a higher radiation dose may be required or that more of the cure speed enhancing photoinitiator is required to further increase the cure speed so that the ink composition is suitably cured at the selected radiation dose.

20                   The undercut test denotes whether the sample disintegrated after the MEK rub test.

The test sample showed 200 MEK (rubs), no unreacted composition and no undercut.

25   Example II and III, and Comparative Example A

Two radiation-curable carrier systems were first formed by combining the components shown in Tables 2 and 3.



Table 2  
Carrier System AA

Component	Amount (% by weight of total system)
Epoxy Acrylate Monomer	33.9
Aliphatic Urethane Diacrylate Oligomer	19.9
Pentaerythritol Tetra-acrylate	9.95
Isobornyl Acrylate	3.06
Phenoxy Ethyl Acrylate	3.06
1,6-Hexanediol Diacrylate	13.64
Silicone Diacrylate	1.14
2,6-di-tert-Butyl-Methyl-Phenol	0.57
2-Methyl-1-(4-(Methylthio)phenyl)- 2-(4-Morpholinyl)-1-Propanone	4.55
Ink Sure Speed Enhancing Photoinitiator CGI 819	1.14
Acrylated Benzophenone	9.09

Table 3

## Carrier System BB

Component	Amount (% by weight of total system)
Epoxy Acrylate monomer	35.93
Aliphatic Urethane Diacrylate Oligomer	21.14
Pentaerythritol Tetra-acrylate	10.55
Isobornyl Acrylate	3.24
Phenoxy Ethyl Acrylate	3.24
1,6-Hexanediol Diacrylate	11.52
Silicone Diacrylate	2.31
2,6-di-tert-Butyl-Methyl-Phenol	0.58
Phosphine Oxide, Di-Phenyl(2,4,6-Trimethyl Benzoyl)	11.52

The radiation-curable carrier system AA was combined with the pigments shown in Table 4 to form radiation-curable ink compositions. The radiation-curable carrier system BB was combined with the pigments shown in Table 5 to form radiation-curable ink compositions. For comparison, commercially available ink coating compositions shown in Table 6 were utilized (comparison experiment A).

20 micron thick drawdowns of the ink compositions were formed on mylar films and then exposed to 0.1 J/cm<sup>2</sup> UV light to form sample films. The properties of the films was tested and the results are shown in Tables 4 through 6.

Table 4

Component (weight % based on total weight of composition)	White	Red	Violet	Yellow	Rose	Black	Slate	Orange	Blue	Green	Brown	Aqua
Radiation-Curable Carrier System (A)	86.37	78.14	83.77	79.80	83.00	89.29	88.27	81.64	88.00	85.5	81.79	85.35
Pigment	13.63	21.86	16.23	20.20	17.00	10.71	11.73	18.36	12.00	14.50	18.21	14.65
Test Results												
Viscosity (mPa.s)	2410	1920	2150	2140	2260	2300	2440	2280	2420	2180	2300	2265
MEK (rubs)	200+	200+	200+	200+	200+	200+	170	200+	130	200+	200+	200+
							200		190			
Release From Matrix Material	pass	pass	slight zipper	pass	pass	pass	pass	pass	pass	pass	pass	pass
Adhesion to Secondary Coating	good	good	good	good	good	good	good	good	good	good	good	good
RAU in N <sub>2</sub> (%)	75	74	77	83	84	83	81	83	80	81	79	79
RAU in O <sub>2</sub> (%)	73	67	73	79	78	79	77	78	75	77	75	75

Average RAU in N<sub>2</sub> (%) was 80

Average RAU in air (%) was 76.

Table 5

Component (weight % based on total weight of composition)	White	Red	Violet	Yellow	Rose	Black	Slate	Orange	Blue	Green	Brown	Aqua
Radiation-Curable Carrier System (A)	85.01	75.96	82.14	77.78	81.30	88.22	87.10	79.81	86.80	84.05	79.97	83.14
Pigment	14.99	24.04	17.86	22.22	18.70	11.78	12.90	20.19	13.2	15.95	20.03	16.86
Test Results												
Viscosity (mPa.s)	2420	1980	2120	2250	2260	2280	2474	2300	2370	2260	2200	2320
MEK (rubs)	200+	200+	200+	200+	200+	200+	200+	200+	200+	200+	200+	200+
Release From Matrix Material	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass
Adhesion to Secondary Coating	good	good	good	good	good	good	good	good	good	good	good	good
RAU in N <sub>2</sub> (%)	87	81	87	85	87	88	89	87	89	86	88	89
RAU in air (%)	80	69	74	74	78	78	79	75	78	76	74	79

Average RAU in N<sub>2</sub> was 87; average RAU in air (%) was 79

Table 6

Test Results	White	Red	Violet	Yellow	Rose	Black	Slate	Orange	Blue	Green	Brown	Aqua
MEK (rubs)	200	200	155	108	200	180	155	145	133	200	185	135
Release From Matrix	poor	poor	poor	poor	poor	poor	poor	poor	poor	poor	poor	poor
Material												
Adhesion to Secondary	good	good	good	good	good	good	good	good	good	good	good	good
Coating												
RAU in N <sub>2</sub> (%)	69	71	70	74	78	80	78	79	70	74	74	65
RAU in air (%)	54	68	74	72	73	78	77	77	57	75	73	56

Average RAU in N<sub>2</sub> (%) was 74

Average RAU in air (%) was 70

By comparing the test results of Tables 4 and 5 with Table 6, it can be easily observed that the presence of a suitable photoinitiator provided a dramatic increase in the average %RAU, when curing in the presence and absence of oxygen. It can also be observed that the presence of a suitable photoinitiator provided the ink coating with good adhesion to the outer primary coating in combination with providing good release from the matrix material even when cured at a low irradiation dose. Thus, the ink coatings formed according to the present invention are suitable for use in a ribbon assembly when break-out of the individual coated optical glass fibers is desired.

#### Example IV

An ink coating composition was prepared by mixing the following components:

Component:	Percent by weight of total composition:
Ebecryl 3700 (epoxy acrylate)	51.0
alkoxylated aliphatic diacrylate	30.0
Irgacure 819 <sup>1</sup>	1.0
Irgacure 907	3.0
Benzophenone	4.0
Blue pigment (Penn Color)	1.5
BYK 333 <sup>2</sup>	0.5

<sup>1</sup> Irgacure 819 is supplied by Ciba Geigy

<sup>2</sup> BYK 333 is a polyether modified dimethyl polysiloxane.

Example v

Another ink coating composition was prepared by mixing the following components:

5	Component:	Percent by weight of total composition:
	polyether urethane acrylate:	
	PTMG/TDI/HEA <sup>1</sup>	60.0
10	ethoxylated bisphenol-A diacrylate	25.0
	N-vinyl caprolactam	25.0
	trimethylolpropanetri-acrylate	4.0
	Lucirin TPO <sup>2</sup>	2.0
	Benzophenone	3.5
15	Blue pigment (Penn Color)	1.5
	silicone oil <sup>3</sup>	0.5

<sup>1</sup> reaction product of polytetramethylene glycol, toluene diisocyanate and hydroxyethyl acrylate

20 <sup>2</sup> 2,4,6-trimethylbenzoyldiphenylphosphine oxide  
[Lucirin TPO by BASF]

<sup>3</sup> silicone oil = Dow Corning 57/Dow Corning 190 mixture, whereby

25 Dow Corning 57: polyether modified dimethyl polysiloxane, and  
Dow Corning 190: siliconeglycol copolymer

30 To test the ink compositions, glass plates were coated with a 75 micron thick, outer primary coating which was cured with a D-lamp (1 J/cm<sup>2</sup>). Next, the 75 micron thick drawdowns of the ink compositions, shown in examples IV and V, were applied to coated glass plates, and then

irradiated with ultraviolet light by a combination of a D lamp with an energy of 1000 mJ/cm<sup>2</sup> in the wavelength area up to 450 nm and a H lamp with an energy of 500 mJ/cm<sup>2</sup> in the wavelength area from 200 to 400 nm to produce cured ink films.

With these test plates, the adhesion of the ink to the outer primary coating was determined.

In order to test the adhesion (or break-out) of the matrix material from the inks, coated and inked glass plates were used, and a matrix material was coated thereon. The matrix was cured with a D-lamp at 1 J/cm<sup>2</sup>.

The energy output of the D and the H lamp were measured by a EIT UV-cure light bug.

The cured inks, described in the examples IV and V, showed a good adhesion to the outer primary coating, and the matrix showed a good break-out from the ink layers.

#### Test procedures

The adhesion strenght of the cured ink coating and peelability of the matrix material were measured using the following methods:

##### (1) Adhesion strenght

The ink compositions, as were applied to an outer primary coating, were cut into with a knife in order to evaluate whether a good adhesion was obtained or not. A good adhesion was denoted as (+), a bad adhesion as (-); intermediate values were given ratings with (+) and (-).



(2) Peelability test

The peelability of the matrix material from the ink composition was judged. The cured films were cut into with a knife in order to evaluate whether a good break-out was obtained or not. The peelability of the matrix material from the ink layer was evaluated by observation of the samples using the naked eye and touching the samples with the finger to examine the presence or absence of residues of the matrix on the ink layer. If neither observation confirmed any residues remaining on the ink coating when pulling away the matrix/ribbon material, the peelability was judged as good (+); if the presence of the matrix was confirmed or if the ink layer remained to the matrix, the peelability was judged as bad (-).

The following test examples were studied and the results of the test procedures are given in Table 7:

Comparitive example B:

The composition of Example II without benzophenone.

Example V: as described above

Example VI:

The composition of Example V + 3% Ebecryl 350 wherein Ebecryl 350 (UCB-Radcure) is an acrylated silicone (difunctional).

Example VII

The composition, which can be used as a colored secondary coating, was prepared by mixing the following ingredients.

5

Component:	Percent by weight of total composition:
------------	--

	polyester based urethane acrylate	22
10	polyether based urethane acrylate	20
	isobornyl acrylate	14
	ethoxylated TMPTA	17
	ethoxylated bisphenol A diacrylate	16
15	Irgacure 907	3
	Irgacure 819	1
	Blue pigment (Penn Color)	1
	Titanium dioxide	2
	1,6-hexamethylene diacrylate	3
20	benzophenone	4

Table 7

	Release (of the matrix from the ink)	Adhesion (of the ink to the outer primary coating)
25		
	B ---	+
30	V ++	+-
	VI ++	+++
	VII ++	+-

The use of benzophenone alone results in a good break-out. Ebecryl 350 does not improve this substantially, but nevertheless, decreases the adhesion of the ink coating to the outer primary coating. In other words, it is preferred not to use considerable amounts of release agents (such as Ebecryl 350) as this reduces the adhesion strength of the ink coating on the outer primary coating.

Furthermore, these experiments show that benzophenone substantially improves the break-out of the matrix material from different ink types.

#### Example VIII

75 micron thick drawdowns of two commercially available radiation-curable outer primary coating compositions were cured on Mylar sheets by exposure to 1.0 J/cm<sup>2</sup> UV radiation to form outer primary films. Samples were made by cutting the cured films into 2 inch by 2 inch squares. The samples were then placed in a desiccator for a minimum of 15 minutes. The initial weight of each of the samples was measured. 3 samples were submerged into each of eight different monomers and weighed at intervals of 1 second, 5 seconds, 10 seconds and 30 seconds (total elapsed time). The percent weight change of each of the samples and the average weight change of the three samples for each monomer was calculated and the results are shown in Table 8.

Table 8

	Commercial Outer Primary Coating No. 1					Commercial Outer Primary Coating No. 2				
	Percent Change In Weight After 30					Percent Change in Weight After 30				
	Seconds					Seconds				
Monomer	Samp. 1	Samp. 2	Samp. 3	Average		Samp. 1	Samp. 2	Samp. 3	Average	
HDDA	+ .58	+ .58	+ .39	+ .52		+ .52	+ .58	+ .39	+ .5	
BPAEDA	+ .8	+ 1.13	+ 1.14	+ 1.02		+ .46	+ .37	+ .33	+ .39	
SA1002	+ 1.03	+ .46	+ .64	+ .71		+ .98	+ .26	+ .75	+ .66	
IBOA	+ .25	+ .37	+ .26	+ .29		+ .43	+ .25	+ .11	+ .26	
SR504A	+ 1.14	+ .87	+ .19	+ .73		+ .14	+ .48	+ .27	+ .3	
PEA	+ .8	+ .88	+ .93	+ .87		+ .85	+ .56	+ .37	+ .59	
n-Vinyl Formamide	+ 2.32	+ 2.91	+ 3.11	+ 2.78		+ 2.71	+ 2.72	+ 3.21	+ 2.88	
IDA	+ .23	+ .25	+ .30	+ .30		+ .14	+ .11	+ .33	+ .19	
	Percent Change in Weight After 10					Percent Change in Weight After 10				
	Seconds					Seconds				
Monomer	Samp. 1	Samp. 2	Samp. 3	Average		Samp. 1	Samp. 2	Samp. 3	Average	
HDDA	+ .55	+ .75	+ .22	+ .51		+ .72	+ .38	+ .55	+ .55	
BPAEDA	+ 1.24	+ .65	+ .58	+ .82		+ .33	+ .44	+ .3	+ .36	

-51-

SA1002	+ .53	+ .46	+ .38	+ .46	+ .29	+ .33	+ .82	+ .48
IBOA	+ .31	+ .35	+ .29	+ .32	+ .24	+ .03	+ .5	+ .26
SR504A	+ .76	+ .33	+ .31	+ .53	+ .09	+ .42	+ .27	+ .26
PEA	+ .74	+ .38	+ .55	+ .66	+ .75	+ .32	+ .42	+ .5
n-Vinyl Formamide	+ 1.69	+ 2.31	+ 2.54	+ 2.18	+ 1.97	+ 1.96	+ 2.62	+ 2.18
IDA	+ .26	+ .28	+ .30	+ .28	+ .14	+ .08	+ .18	+ .13
Percent Change in Weight After 5								
Seconds								
Monomer	Samp. 1	Samp. 2	Samp. 3	Average	Samp. 1	Samp. 2	Samp. 3	Average
HDDA	+ .78	+ .54	+ .27	+ .53	+ .8	+ .61	+ .71	+ .71
BPAEDA	+ .93	+ 1.07	+ .74	+ .91	+ .26	+ .37	+ .33	+ .32
SA1002	+ .87	+ .46	+ .29	+ .54	+ .53	+ .51	+ .58	+ .54
IBOA	+ .2	+ .32	+ .19	+ .24	+ .34	+ .34	+ .22	+ .3
SR504A	+ 1.83	+ .76	+ .31	+ .97	+ .26	+ .28	+ .27	+ .27
PEA	+ .67	+ .41	+ .24	+ .44	+ .5	+ .6	+ .48	+ .53
n-Vinyl Formamide	+ 1.13	+ 1.92	+ 1.69	+ 1.58	+ 1.44	+ 1.34	+ 2.02	+ 1.6
IDA	+ .2	+ .14	+ .15	+ .16	+ .21	+ .14	+ .22	+ .19

-52-

	Percent Change in Weight After 1 Second					Percent Change in Weight After 1 Second				
HDDA	+ .45	+ .4	+ .17	+ .34		+ .88	+ .46	+ .39	+ .58	
BPAEDA	+ .65	+ 1.1	+ 1.07	+ .94		+ .26	+ .3	+ .33	+ .3	
SA1002	+ .87	+ .62	+ .44	+ .94		+ .37	+ .29	+ .58	+ .41	
IBOA	+ .28	+ .4	+ .42	+ .37		+ .3	+ .28	+ .11	+ .23	
SR504A	+ 1.03	+ .64	+ .31	+ .66		+ .26	+ .11	+ .17	+ .18	
PEA	+ .43	+ .24	+ .38	+ .35		+ .46	+ .35	+ .34	+ .38	
n-Vinyl Formamide	+ .59	+ .73	+ .98	+ .77		+ .49	+ .59	+ 1.05	+ .71	
IDA	+ .2	+ .25	+ .11	+ .19		+ .14	+ .14	+ .15	+ .14	

The test results in Table 8 demonstrate that the monomers present in radiation-curable ink compositions exhibit different levels of adsorption into different commercially available outer primary coatings. In general, the greater the adsorption into the outer primary coating, the greater the resulting adhesion between the cured ink coating and the outer primary coating.

## 10 Test Procedures

### %RAU

This is an FTIR method for determining the degree of cure on the surface of a coating to a depth of 1 to 3  $\mu\text{m}$ , following exposure to a predetermined dose of UV radiation. A drawdown of the sample material is first formed on a glass plate. The drawdown is then exposed to the predetermined dose of UV radiation to cure the drawdown and form a coating. The coating is cut into strips, approximately 10 mm by 50 mm.

An infrared spectrum of the uncured, liquid sample and an infrared spectrum of the cured sample are obtained. Infrared spectrometry is now well known and any infrared spectrometer can be utilized to obtain the infrared spectrum.

The net peak area of the acrylate unsaturation absorbance for the uncured liquid sample is measured. For most acrylate-based coatings, the absorbance at about  $810\text{ cm}^{-1}$  should be used. However, if the coating contains a siloxane or other component

which absorbs strongly at or near  $810\text{ cm}^{-1}$ , an alternative acrylate absorbance peak can be used. The absorbances at about  $1410\text{ cm}^{-1}$  and about  $1635\text{ cm}^{-1}$  have been found to be satisfactory. The net peak area can  
5 be measured using the well known baseline technique in which a baseline is drawn tangent to absorbance minima on either side of the peak. The area above the baseline and under the peak is the net peak area.

A reference area is then determined. The  
10 reference absorbance should not change in intensity as the liquid sample is cured. Many formulations have an absorbance in the range of about  $780$  to about  $750\text{ cm}^{-1}$  that can be used as a reference absorbance. The net peak area of the reference absorbance is measured.

15 The ratio of the acrylate absorbance to the reference absorbance for the uncured, liquid sample is determined using the following formula:

$$R_L = A_{AL} / A_{RL}$$

20

where

$A_{AL}$  is the net peak area of the acrylate absorbance,  
 $A_{RL}$  is the net peak area of the reference absorbance,  
and

25  $R_L$  is the area ratio for the liquid sample.

The ratio of the acrylate absorbance to the reference absorbance for the cured sample is determined using the following formula:

30

$$R_C = A_{AC} / A_{RC}$$



where

$A_{AC}$  is the net peak area of the acrylate absorbance,

$A_{RC}$  is the net peak area of the reference absorbance,

5 and

$R_C$  is the area ratio for the cured sample.

The degree of cure as a percent reacted  
acrylate unsaturation (%RAU) is determined using the  
10 following formula:

$$\%RAU = [(R_L - R_C) \times 100\%] / R_L$$

15 **MEK rub Test**

The test procedures described in ASTM D  
4752 was followed with the following exception. Light  
finger pressure was used on the material being rubbed  
against the test sample.

20

While the claimed invention has been  
described in detail and with reference to specific  
embodiments thereof, it will be apparent to one of  
ordinary skill in the art that various changes and  
25 modifications can be made to the claimed invention  
without departing from the spirit and scope thereof.

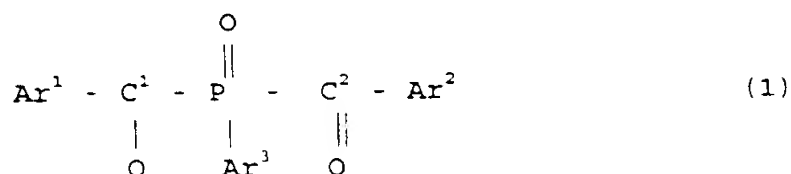
C L A I M S:

1. A ribbon assembly having the functional  
5 capability of providing break-out of color coded  
optical glass fibers from said ribbon assembly,  
said ribbon assembly comprising:  
a plurality of coated optical glass fibers;  
having an ink or colored secondary coating on at  
10 least one of said coated optical glass fibers;  
and  
a matrix material binding said plurality of  
coated optical fibers together, wherein said  
colored coating being formed from a radiation  
15 curable coating composition comprising:  
a radiation-curable carrier system  
containing a mixture of radiation-curable  
monomers and oligomers and at least one  
photoinitiator; and  
20 a pigment dispersed in said radiation-  
curable carrier system, wherein said  
monomers, oligomers and photoinitiator are  
selected to provide  
an average percentage of reacted acrylate  
25 unsaturation which provides a level of  
adhesion between said matrix material and  
said colored coating that is less than a  
level of adhesion between said ink coating  
and said coated optical glass fiber to  
30 provide break-out of said color coded  
optical glass fiber from said ribbon

assembly when said ink coating composition  
is cured by exposure to a suitable  
ultraviolet radiation dose.

2. A ribbon assembly according to claim 1, wherein  
5 the suitable radiation dose is about 0.125 joules  
per square centimeter.
3. A ribbon assembly according to any one of claims  
1-2, wherein the colored coating is an ink  
coating adjacent to an outer primary coating.
- 10 4. A ribbon assembly according to any one of claims  
1-3, wherein said colored coating having said  
degree of cure which provides an MEK value of at  
least 100 rubs when cured by exposure to  
ultraviolet radiation.
- 15 5. A ribbon assembly according to any one of claims  
1-4, wherein said ink coating having said degree  
of cure which provides an MEK value of at least  
200 rubs when cured by exposure to ultraviolet  
radiation.
- 20 6. A ribbon assembly according to any one of claims  
1-5, wherein said photoinitiator comprises at  
least one compound according to formula (1):

25



30

wherein:

Ar represents a carbon containing compound having  
at least one aromatic functional group;

P is bonded directly to an aromatic functional group present in  $Ar^3$ ;  
 $C^1$  is bonded directly to an aromatic functional group present in  $Ar^1$ ; and  
5  $C^2$  is bonded directly to an aromatic functional group present in  $Ar^2$ , and wherein at least one of the carbon containing compounds Ar has a molecular weight and molecular structure that is capable of forming at least one of the following  
10 free-radicals upon exposure to ultraviolet radiation:

$Ar^1-C^1O\cdot$ ;

$Ar^2-C^2O\cdot$ ; or

$Ar^3-PO\cdot$ .

- 15 7. A ribbon assembly according to claim 6, wherein all three carbon containing compounds Ar have a molecular weight and molecular structure that is capable of forming said free-radicals.
8. A ribbon assembly according to any one of claims  
20 1-7, wherein said ink coating having an average percentage of reacted acrylate unsaturation of at least 75% when said radiation-curable ink coating composition is cured by exposure to an  
25 ultraviolet radiation dose of about 0.125 joules per square centimeter in an inert atmosphere.
9. A ribbon assembly according to claim 6, wherein said ink coating having an average percentage of reacted acrylate unsaturation of at least about 80%.
- 30 10. A ribbon assembly according to any one of claims 1-7, wherein said ink coating having an average

percentage of reacted acrylate unsaturation of at least 70% when said radiation-curable ink coating composition is cured by exposure to an ultraviolet radiation dose of about 0.1 joules per square centimeter in an oxygen containing atmosphere.

5  
11. A ribbon assembly according to claim 9, wherein said ink coating having an average percentage of reacted acrylate unsaturated of at least about  
10 75%.

12. A ribbon assembly according to any one of claims 1-11, wherein said average percentage of reacted acrylate unsaturation is based on a measured percentage of reacted acrylate unsaturation for  
15 at least 6 different colored ink compositions each formulated from the same radiation-curable carrier system and containing different colored pigments.

13. A ribbon assembly according to claim 12, wherein  
20 said average percentage of reacted acrylate unsaturation for at least 12 different colored ink compositions each formulated from the same radiation-curable carrier system and containing different colored pigments.

25 14. A radiation-curable ink coating composition adapted to provide a color coding in the ribbon assembly of claim 1 comprising

- a) an oligomer having at least one radiation curable group
- 30 b) a reactive diluent
- c) at least about 1 wt.% of homolytic photoinitiator for radical polymerisation

d) a pigment, and

e) additives

wherein the composition comprises an effective amount of a benzophenone-type compound.

5 15. A composition according to claim 14 wherein a benzophenone-type compound is an organic compound with a molecular weight between 170 and 500, consisting essentially of benzophenone or a substituted benzophenone group.

10 16. A composition according to any one of claims 14-15, wherein a benzophenone-type compound is not a ring-bonded benzophenone.

17. A composition according to any one of claims 14-16, wherein compound e) comprises at least a  
15 lubricant.

18. A radiation-curable ink composition according to any one of claims 14-17, adapted for coating optical glass fibers and being formulated from a composition comprising:

20 from about 20 to about 70 weight % of at least one radiation-curable oligomer;

from about 5 to about 80 weight % of at least one radiation-curable diluent;

25 from about 4 to about 20 weight % of a homolytic photoinitiator;

from about 1 to about 20 weight % of a pigment;

and more than about 2 weight % of a benzophenone-type compound;

30 wherein said weight % is with respect to the total weight of said radiation-curable ink composition.

19. A method for curing an ink composition according to any one of claims 14-18 on a coated optical fiber, wherein the composition is cured with a combination of a D and a H lamp.

20. A coated and colored optical glass fiber,  
comprising:  
an optical glass fiber;  
an inner primary coating adjacent to the surface  
5 of said optical glass fiber;  
an outer primary coating adjacent to the surface  
of said inner primary coating; and  
an ink coating adjacent to the surface of said  
outer primary coating, wherein the ink coating is  
10 the cured ink coating composition, according to  
any one of claims 14-18.
21. A coated and colored optical glass fiber,  
comprising:  
an optical glass fiber;  
15 an inner primary coating adjacent to the surface  
of said optical glass fiber;  
a colored outer primary coating adjacent to the  
surface of said inner primary coating wherein the  
outer primary coating is the cured ink coating  
20 composition according to any one of claims 14-18.
22. A ribbon assembly comprising:  
a plurality of coated optical glass fibers; and  
a matrix material which binds said plurality of  
coated optical glass fibers together, wherein at  
25 least one of said coated optical glass fibers  
comprises a coated and colored optical glass fiber  
according to claim 20-21.
23. A ribbon assembly according to claim 1 comprising:  
a plurality of coated optical glass fibers; and  
30 a matrix material which binds said plurality of  
coated optical glass fibers together, wherein at  
least one of said coated optical glass fibers  
comprises:  
an optical glass fiber;

an inner primary coating adjacent to a surface of said optical glass fiber;  
an outer primary coating adjacent to a surface of an inner primary coating; and  
5 an ink coating adjacent to a surface of said outer primary coating, wherein said ink coating being formed from a radiation-curable ink coating composition containing a monomer selected to be adsorbable into said outer  
10 primary coating to a degree which when suitably cured provides a level of adhesion between said ink coating and said outer primary coating that is greater than a level of adhesion between said ink coating and said  
15 matrix material.

24. A ribbon assembly according to claim 23, wherein said monomer exhibits an outer primary coating adsorption index of at least 7.
25. A ribbon assembly according to claim 24, wherein  
20 said monomer exhibits an outer primary coating adsorption index of at least 10.
26. A radiation-curable ink coating composition adapted to provide a color coding in the ribbon assembly of claim 1, said ink coating composition  
25 comprising:  
a radiation-curable carrier system containing a mixture of radiation-curable monomers and oligomers and at least one photoinitiator, wherein  
said monomers, oligomers and photoinitiator are  
30 selected to provide an average percentage of reacted acrylate unsaturation of greater than 70% when cured by exposure an ultraviolet radiation dose of about 0.125 joules per square centimeter in an oxygen containing atmosphere and applied at



a thickness of from about 3 to about 10 microns;  
and

at least one pigment dispersed within said  
radiation-curable carrier system.

- 5    27. A radiation-curable ink coating composition  
adapted to provide a color coding in the ribbon  
assembly of claim 1, said ink coating composition  
comprising:

10    a radiation-curable carrier system containing at  
least one monomer having an outer primary coating  
adorption index of at least 5, at least one  
oligomer, and at least one photoinitiator; and  
at least one pigment dispersed within said  
radiation-curable carrier system.

# INTERNATIONAL SEARCH REPORT

International Application No

PCT/NL 98/00254

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 C03C25/02 G02B6/44 C09D11/10

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 C03C C09D G02B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No
X	EP 0 699 933 A (AT & T CORP) 6 March 1996  see page 4, line 5 - page 5, line 38 ---	1-5, 8-17, 19-27
A	WO 90 13579 A (DESOTO INC) 15 November 1990 see claims ---	1,6,7
A	GB 2 259 704 A (CIBA GEIGY AG) 24 March 1993 see page 10, last line, paragraph 3; claims ---	1,6,7
A	EP 0 615 980 A (CIBA GEIGY AG) 21 September 1994 see claims ---	1,6,7
	--- -/--	

☒ Further documents are listed in the continuation of box C

☒ Patent family members are listed in annex

### Special categories of cited documents

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken as a whole

"Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"Z" document member of the same patent family

Date of the actual completion of the international search

20 August 1998

Date of mailing of the international search report

27/08/1998

Name and mailing address of the ISA

European Patent Office, P.B. 5815 Patentlaan 2

NL - 2280 HV Rijswijk

Tel: (+31-70) 340-2040, Tx: 31 651 eponi

Fax: (+31-70) 340-3016

Authorized officer

Van Bommel, L

# INTERNATIONAL SEARCH REPORT

International Application No  
PCT/NL 98/00254

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category	Citation of document with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	FR 2 672 699 A (ALCATEL CABLE) 14 August 1992 see the whole document ---	1-27
P, A	WO 97 18493 A (LIGHTGUIDE MATERIALS INC) 22 May 1997 see page 3, line 4 - page 10, line 32 ---	1-27
P, A	WO 97 19029 A (DSM NV ; JAPAN SYNTHETIC RUBBER CO LTD (NL); ISHIKAWA MIYUKI (JP);) 29 May 1997 see page 2, line 26 - page 7, line 18 -----	1-27

# INTERNATIONAL SEARCH REPORT

Information on patent family members

i. national Application No

PCT/NL 98/00254

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
EP 0699933	A	06-03-1996	US 5539849 A	23-07-1996
			AU 3028595 A	07-03-1996
			CA 2156874 A	27-02-1996
			JP 8068923 A	12-03-1996
			NZ 272863 A	24-02-1997
WO 9013579	A	15-11-1990	AT 115610 T	15-12-1994
			AU 629350 B	01-10-1992
			AU 5636290 A	29-11-1990
			CA 2016547 A	12-11-1990
			DE 69015181 D	26-01-1995
			DE 69015181 T	20-07-1995
			EP 0473643 A	11-03-1992
GB 2259704	A	24-03-1993	JP 5505202 T	05-08-1993
			CH 682666 A	29-10-1993
			AT 401265 B	25-07-1996
			AT 188592 A	15-12-1995
			AU 655675 B	05-01-1995
			AU 2525192 A	01-04-1993
			BE 1006011 A	19-04-1994
			CA 2078722 A	24-03-1993
			DE 4231579 A	25-03-1993
			ES 2050607 A	16-05-1994
			FR 2681599 A	26-03-1993
			IT 1255509 B	09-11-1995
			JP 5345790 A	27-12-1993
			MX 9205345 A	01-04-1993
			NL 9201641 A	16-04-1993
			SE 503060 C	18-03-1996
			SE 9202668 A	24-03-1993
			RU 2091385 C	27-09-1997
			US 5472992 A	05-12-1995
			US 5399770 A	21-03-1995
			ZA 9207226 A	23-03-1993
EP 0615980	A	21-09-1994	AU 682334 B	02-10-1997
			AU 5775394 A	22-09-1994
			BR 9401197 A	18-10-1994
			CA 2119206 A	19-09-1994

# INTERNATIONAL SEARCH REPORT

Information on patent family members

national Application No

PCT/NL 98/00254

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP 0615980 A		JP 6298818 A US 5534559 A ZA 9401879 A	25-10-1994 09-07-1996 19-09-1994
FR 2672699 A	14-08-1992	NONE	
WO 9718493 A	22-05-1997	AU 7554496 A	05-06-1997
WO 9719029 A	29-05-1997	JP 9142889 A AU 7590696 A	03-06-1997 11-06-1997



[ SUGHRUE, MION, ZINN, MACPEAK  
& SEAS, PLLC  
Attn. Hannon, Brian, W.  
2100 Pennsylvania Avenue, N.W.  
Suite 800  
Washington, D.C. 20037-3213  
UNITED STATES OF AMERICA ]

[ Date: 13/12/2001 ]

